

TITLE OF THE INVENTION

Multi-Piece Solid Golf Ball

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CROSS REFERENCE TO RELATED APPLICATION

This application is an application files under 35  
U.S.C. § 111(a) claiming benefit pursuant to 35 U.S.C. §  
10 119(e)(i) of the filing date of the Provincial Application  
60/058,563 filed on September 11, 1997 pursuant to 35  
U.S.C. § 111(b).

BACKGROUND OF THE INVENTION

15 Field of the Invention

This invention relates to a multi-piece solid golf ball having a cover of inner and outer layers and more particularly, to a multi-piece solid golf ball in which cover hardness and dimples are optimized ~~so as~~ to improve 20 flight distance performance.

Prior Art

Golf balls are generally classified into solid golf balls in which a solid core is enclosed with at least one 25 layer of cover and wound golf balls in which a wound core in the form of a center ball having thread rubber wound thereon is enclosed with a cover. Numerous modifications were heretofore proposed to improve flight distance properties, spin performance, and controllability.

As one example of such proposals, an approach of increasing a spin rate by forming the cover soft or to low 30 hardness falls under the category of the prior art. In particular, improvements in multi-piece solid golf balls are by adjusting the composition and hardness of the 35 thermoplastic resin of which each cover layer is constructed. For example, if it is desired to increase a

spin rate, the outer cover layer coming in direct contact with the club face is formed relatively soft in consideration of a friction phenomenon upon impact. Inversely, if it is desired to decrease a spin rate, the 5 outer cover layer is formed relatively hard.

However, the multi-piece solid golf balls wherein the outer cover layer is formed relatively soft have the problem that a desired spin rate is not always obtained because the hardness of the inner cover layer in contact 10 with the outer cover layer is not optimized <sup>Therefore</sup> and thus, the deformation process upon impact differs among the respective layers.

Also proposed were techniques of forming the inner cover layer relatively soft in order to increase a spin 15 rate and forming the outer and inner cover layers relatively soft in order to further increase a spin rate. There arises the problem that the trajectory changes in flight to adversely affect the flight distance.

On the other hand, for those golf balls required to 20 have flight distance performance, it is difficult to form dimples suitable for the spin range and restitution which vary with the cover hardness. Golf balls with dimples of one type suffer from the problem that they rise too high or drop to detract from ~~the~~ flight distance performance.

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#### SUMMARY OF THE INVENTION

The present invention has been made under the above-mentioned circumstances and its object is to provide a golf ball comprising a solid core enclosed with two inner 30 and outer layers enabling <sup>an</sup> ~~to~~ increase <sup>of</sup> ~~a~~ flight distance.

Making extensive investigations to achieve the above object, <sup>The Inventor</sup> ~~we~~ have found in connection with a multi-piece solid golf ball comprising a solid core and a cover of two inner and outer layers surrounding the core, the outer 35 cover layer being formed in the surface with a plurality of dimples, that a spin rate is approximately explained in terms of a product of the Shore D hardness of the inner

cover layer multiplied by the Shore D hardness of the outer cover layer. More particularly, a more spin rate is obtained when the product of the Shore D hardnesses of the inner and outer layers has a relatively smaller value.

5 Inversely, a ~~less~~ spin rate is obtained when the same product has a relatively larger value. Accordingly, one effective means for taking full advantage of the spin property dependent on the product of the Shore D hardnesses of the inner and outer layers and improving the flight performance of the golf ball is to divide the range of the product into sub-ranges and form dimples so as to satisfy the following two requirements associated with the sub-ranges of the product. More particularly, it has been found effective as a first requirement to specify a

10 proportion  $V_R$  (%) of the total of the volumes of dimple spaces each defined below a plane circumscribed by the dimple edge to the overall volume of a phantom sphere given on the assumption that the golf ball surface is free of dimples. ~~and as a second requirement~~ to form at least

15 three types of dimples which are different in at least one of a diameter, a depth, and a value  $V_0$  which is the volume of one dimple space defined below a plane circumscribed by the dimple edge divided by the volume of a cylinder whose bottom is the plane and whose height is the maximum depth of the dimple from the bottom. <sup>The Inventors</sup> We have also found that to

20 specify the distortion of the solid core and to specify the Shore D hardness of the inner and outer cover layers are more effective. The present invention is predicated on this finding.

25 30 Specifically, the present invention provides:

1) A multi-piece solid golf ball comprising a solid core and a cover of two inner and outer layers surrounding the core, the outer cover layer having a surface formed with a plurality of dimples, characterized in that

35 a product of the Shore D hardness of said inner cover layer multiplied by the Shore D hardness of said outer cover layer and a proportion  $V_R$  (%) of the total of the

volumes of dimple spaces each defined below a plane circumscribed by the dimple edge to the overall volume of a phantom sphere given on the assumption that the golf ball surface is free of dimples satisfy any one of the  
5 following combinations (1) to (5):

(1) the product of Shore D hardnesses of inner and outer cover layers: 1,500 to less than 2,000

$V_R$ : 0.8 to 1.1%

10 (2) the product of Shore D hardnesses of inner and outer cover layers: 2,000 to less than 2,500

$V_R$ : 0.75 to 1.05%

(3) the product of Shore D hardnesses of inner and outer cover layers: 2,500 to less than 3,000

$V_R$ : 0.7 to 1%

15 (4) the product of Shore D hardnesses of inner and outer cover layers: 3,000 to less than 3,500

$V_R$ : 0.65 to 0.95%

(5) the product of Shore D hardnesses of inner and outer cover layers: 3,500 to 4,000

20  $V_R$ : 0.6 to 0.9%,

and said dimples include at least three types of dimples which are different in at least one of a diameter, a depth, and a value  $V_0$  which is the volume of one dimple space defined below a plane circumscribed by the dimple edge divided by the volume of a cylinder whose bottom is the plane and whose height is the maximum depth of the dimple from the bottom.

25 2) The multi-piece solid golf ball of 1) wherein the solid core has a distortion of 2.6 to 6.5 mm under an applied load of 100 kg.

30 3) The multi-piece solid golf ball of 1) or 2) wherein both the hardnesses of the inner and outer cover layers are up to 63 in Shore D hardness.

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#### BRIEF DESCRIPTION OF THE DRAWINGS

FIG. 1 is a cross-sectional view of a dimple illustrating how to calculate a value  $V_0$ .

FIG. 2 is a perspective view of the dimple illustrating how to calculate a value  $V_0$ .

FIG. 3 is a cross-sectional view of the dimple illustrating how to calculate a value  $V_0$ .

5 *AnswA1→*

+ DETAILED DESCRIPTION OF THE INVENTION

Now the invention ~~is~~ <sup>will now be</sup> described in more detail. The multi-piece solid golf ball of the invention is defined as comprising a solid core <sup>20</sup> and a cover of <sup>20</sup> two inner and <sup>3n</sup> outer layers <sup>14,16</sup> surrounding the core, the outer cover layer having a surface formed with a plurality of dimples <sup>1</sup>. When the range of the product of the Shore D hardnesses of the inner and outer cover layers is divided into sub-ranges, a dimple parameter can be specified in conjunction with each of the sub-ranges of the product for achieving optimization.

First, the solid core <sup>1</sup> is described. The solid core may be formed of a well-known rubber composition. For example, it is prepared by mixing 1,4-cis-polybutadiene as a base with a well-known crosslinking agent, co-crosslinking agent, filler and so on in a roll mill, introducing a necessary amount of the composition into a solid core-shaping mold, and effecting vulcanization and heat molding. In this regard, the solid core may consist of a single layer or plural layers. In the practice of the invention, the solid core preferably undergoes a distortion or deformation of 2.6 to 6.5 mm, more preferably 2.7 to 6.3 mm, most preferably 2.8 to 6.0 mm under an applied load of 100 kg. A distortion of less than 2.6 mm (hard core) would exacerbate hitting feel. A distortion of more than 6.5 mm (soft core) would result in a ball with less restitution.

The golf ball of the invention is constructed by forming a cover of two (inner and outer) layer structures <sup>14,16</sup> around the aforementioned solid core <sup>20</sup>. The inner and outer layers may be formed of well-known cover stocks.

Specifically, ionomer resins, thermoplastic polyester elastomers, and thermoplastic polyurethane elastomers may be used alone or in admixture of two or more. In the practice of the invention, cover stocks must be selected 5 such that the product of the Shore D hardness of the inner cover layer multiplied by the Shore D hardness of the outer cover layer fall in the range of 1,500 to 4,000.

The Shore D hardnesses of the inner and outer cover layers may be identical with or different from each other 10 insofar as the product of Shore D hardnesses falls in the range of 1,500 to 4,000. That is, the Shore D hardness of the inner cover layer may be substantially identical with the Shore D hardness of the outer cover layer.

Alternatively, either one of the inner and outer cover 15 layers may be softer or harder than the other. The hardness difference between the inner and outer cover layers may be appropriately determined.

Preferably the outer cover layer has a Shore D hardness of up to 63, more preferably 30 to 62, especially 20 35 to 61. With a Shore D hardness of more than 63, there is a risk that no spin is acquired due to a slip phenomenon between the cover and the club face. If the hardness of the outer cover layer is below 30, the ball would lose restitution.

25 On the other than, the inner cover layer preferably has a Shore D hardness of 28 to ~~63~~<sup>63</sup>. Restitution would be lost with an inner cover layer hardness of less than 28 whereas hitting feel would be exacerbated by a hardness above ~~68~~<sup>63</sup>.

30 The method for forming the inner and outer cover layers around the solid core is not critical and can be in accord with conventional ones. Included are a method of enclosing the solid core with a pair of hemispherical half cups of an inner cover layer composition, compression 35 molding to join the cups to the core, placing it in an injection mold, and injecting an outer cover layer composition and another method of forming half cups from

inner and outer cover layer compositions, respectively, mating them to form half cups of the two layer structure, enclosing the solid core with the half cups, and effecting compression molding.

5       The thus formed cover of the inner and outer layers may have any desired gage. Usually the inner cover layer has a gage of 0.5 to 3.0 mm, especially 1.0 to 2.5 mm, the outer cover layer has a gage of 0.5 to 2.5 mm, especially 1.0 to 2.3 mm, and the cover has a total gage of 1.0 to  
10 5.5 mm, preferably 1.5 to 5.0 mm, especially 1.5 to 3.5 mm.

The multi-piece solid golf ball of the invention has a plurality of dimples formed in the outer cover layer. The dimples are formed such that when the product of the 15 Shore D hardness of the inner cover layer multiplied by the Shore D hardness of the outer cover layer is in the range from 1,500 to 4,000, which is divided into sub-ranges, a factor  $V_R$  associated with the dimples, that is, a proportion  $V_R$  (%) of the total of the volumes of dimple spaces each defined below a plane circumscribed by the 20 dimple edge to the overall volume of a phantom sphere given on the assumption that the golf ball surface is free of dimples has the following value.

(1) The product of Shore D hardnesses of inner and outer 25 cover layers: 1,500 to less than 2,000

$$V_R: 0.8 \text{ to } 1.1\%$$

(2) The product of Shore D hardnesses of inner and outer cover layers: 2,000 to less than 2,500

$$V_R: 0.75 \text{ to } 1.05\%$$

30 (3) The product of Shore D hardnesses of inner and outer cover layers: 2,500 to less than 3,000

$$V_R: 0.7 \text{ to } 1\%$$

(4) The product of Shore D hardnesses of inner and outer cover layers: 3,000 to less than 3,500

35       $V_R: 0.65 \text{ to } 0.95\%$

(5) The product of Shore D hardnesses of inner and outer cover layers: 3,500 to 4,000

$V_R$ : 0.6 to 0.9%

More preferred ranges of  $V_R$  are given below.

(1) The product of Shore D hardnesses of inner and outer cover layers: 1,500 to less than 2,000

5        $V_R$ : 0.82 to 1.08%

(2) The product of Shore D hardnesses of inner and outer cover layers: 2,000 to less than 2,500

$V_R$ : 0.77 to 1.03%

10     (3) The product of Shore D hardnesses of inner and outer cover layers: 2,500 to less than 3,000

$V_R$ : 0.72 to 0.98%

(4) The product of Shore D hardnesses of inner and outer cover layers: 3,000 to less than 3,500

$V_R$ : 0.67 to 0.93%

15     (5) The product of Shore D hardnesses of inner and outer cover layers: 3,500 to 4,000

$V_R$ : 0.62 to 0.88%

With respect to the aforementioned range, if the value of  $V_R$  relative to the product of Shore D hardnesses 20 deviates from the specified range, ~~there~~ result <sup>The</sup> ~~is~~ a prematurely falling trajectory and a reduced flight distance.

25     The value  $V_R$  is the sum of volumes  $V_p$  of dimple spaces defined in the golf ball surface to be described later and is calculated according to the following equation:

$$V_R = \frac{V_s}{\frac{4}{3}\pi R^3} \times 100$$

wherein  $V_s$  is the sum of the volumes  $V_p$  of dimple spaces each below a circular plane circumscribed by the dimple edge and  $R$  is a ball radius.

30     It is noted that  $V_s$  in the above equation is represented by the following equation and  $V_R$  can be calculated by substituting the value of  $V_s$  into the above equation of  $V_R$ .

$$V_s = N_1 V_{p_1} + N_2 V_{p_2} + \dots + N_n V_{p_n} = \sum_{i=1}^n N_i V_{p_i}$$

V<sub>p<sub>1</sub></sub>, V<sub>p<sub>2</sub></sub>, ... V<sub>p<sub>n</sub></sub> represent the volumes of dimples of different dimensions and N<sub>1</sub>, N<sub>2</sub>, ... N<sub>n</sub> represent the number 5 of dimples having the volumes V<sub>p<sub>1</sub></sub>, V<sub>p<sub>2</sub></sub>, ... V<sub>p<sub>n</sub></sub>, respectively.

In addition to the above-mentioned requirement of V<sub>R</sub> value, the dimples formed in the golf ball of the invention must further satisfy the requirement that there 10 are included at least three types of dimples which are different in at least one of a diameter, a depth, and a value V<sub>o</sub> which is the volume of one dimple space defined below a plane circumscribed by the dimple edge divided by the volume of a cylinder whose bottom is the plane and 15 whose height is the maximum depth of the dimple from the bottom. If the number of dimple types is less than 3, there arises the problem that the golf ball lofts too high or drops prematurely.

The value V<sub>o</sub> associated with the dimple requirement 20 is described below. In the event that the planar shape of a dimple is circular, as shown in FIG. 1, a phantom sphere 2 having the ball diameter and another phantom sphere 3 having a diameter smaller by 0.16 mm than the ball diameter are drawn in conjunction with a dimple 1. The 25 circumference of the other sphere 3 intersects with the dimple 1 at a point 4. A tangent 5 at intersection 4 intersects with the phantom sphere 2 at a point 6 while a series of intersections 6 define a dimple edge 7. The dimple edge 7 is so defined for the reason that otherwise, 30 the exact position of the dimple edge cannot be determined because the actual edge of the dimple 1 is rounded. The dimple edge 7 circumscribes a plane 8 (circle having a diameter D<sub>m</sub>). Then, the dimple space 9 located below the plane 8 as shown in FIGS. 2 and 3 has a volume V<sub>p</sub>. A 35 cylinder 11 whose bottom is the plane 8 and whose height is the maximum depth D<sub>p</sub> of the dimple from the plane 8 has

a volume  $V_q$ . The ratio  $V_o$  of the dimple space volume  $V_p$  to the cylinder volume  $V_q$  is calculated.

$$V_p = \int_0^{\frac{D_m}{2}} 2\pi xy dx$$

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$$V_q = \frac{\pi D_m^2 D_p}{4}$$

$$V_o = \frac{V_p}{V_q}$$

10 In the event that the planar shape of a dimple is not circular, the maximum diameter or length of a dimple is determined, the plane projected shape of the dimple is assumed to be a circle having a diameter equal to this maximum diameter or length, and  $V_o$  is calculated as above  
15 based on this assumption.

With respect to ~~the~~ <sup>having</sup> dimples of different types according to the invention, dimples of the largest type preferably have a diameter of 3.7 to 4.5 mm, especially 3.8 to 4.3 mm and a depth of 0.15 to 0.25 mm, especially  
20 0.155 to 0.23 mm, and their number is preferably 5 to 80%, especially 10 to 75% of the total dimple number. They are preferably set to have a  $V_o$  value of 0.38 to 0.55. More preferably  $V_o$  is 0.4 to 0.52.

Among the dimples of different types, dimples of the smallest type preferably have a diameter of 2.0 to 3.7 mm, especially 2.4 to 3.6 mm and a depth of 0.08 to 0.23 mm, especially 0.09 to 0.21 mm, and their number is preferably 1 to 40%, especially 2 to 30% of the total dimple number. They are preferably set to have a  $V_o$  value of 0.38 to 0.55, especially 0.4 to 0.52.

The golf ball as a whole should preferably have a  $V_o$  value of 0.38 to 0.55, more preferably 0.4 to 0.52, especially 0.42 to 0.5. A  $V_o$  value of less than 0.38 is likely to lead to a non-long-lasting trajectory whereas a

$V_0$  value of more than 0.55 is likely to lead to a high rise or aloft trajectory.

In the practice of the invention, the total number of dimples is not critical although usually 360 to 460  
5 dimples, especially 370 to 450 dimples are formed.

The golf ball of the invention can be used as tournament golf balls and constructed in accordance with the Rules of Golf to a diameter of not less than 42.67 mm and a weight of not greater than 45.93 grams.

10 The multi-piece solid golf ball of the invention has the advantages that various properties including spin, feeling and durability inherent to the multi-piece construction are further improved and an increased flight distance is expected due to the elimination of a high rise  
15 or dropping trajectory.

#### EXAMPLE

Examples of the present invention are given below together with Comparative Examples by way of illustration  
20 and not by way of limitation.

#### Examples and Comparative Examples

Solid cores having a diameter of 36.7 mm were prepared by mixing a rubber composition of the formulation  
25 shown in Table 1 in a roll mill and heat compression molding the composition at 155°C for 15 minutes.

Each solid core was enclosed with cover stocks shown in Table 2 in the order shown in Tables 4 and 5 to form an inner cover layer and an outer cover layer. The outer  
30 cover layer on the surface was formed with dimples shown in Tables 3, 4, and 5. Three-piece solid golf balls were obtained in this way.

The golf balls thus obtained were examined for flight distance and trajectory by the following tests. The  
35 results are shown in Tables 4 and 5.

#### Flight performance

Using a swing robot by True Temper Co., the ball was hit with a driver at a head speed of 48 m/sec. (#W1/HS48) to measure a spin, carry and total distance.

Trajectory

5       Twelve golf balls of each example were hit under the same conditions as in the flight performance test to visually observe a trajectory.

Table 1

| Solid core composition (pbw)      | I    | II   | III  | IV  |
|-----------------------------------|------|------|------|-----|
| 1,4-polybutadiene (cis structure) | 100  | 100  | 100  | 100 |
| Zinc acrylate                     | 32   | 32   | 23   | 33  |
| Dicumyl peroxide                  | 1.2  | 1.2  | 1.2  | 1.2 |
| Antioxidant                       | 0.1  | 0.1  | 0.1  | 0.1 |
| Zinc oxide                        | 5    | 5    | 5    | 4   |
| Barium sulfate                    | 13.2 | 23.1 | 26.8 | 0   |
| Peptizer                          | 1    | 1    | 1    | 0   |

10

Table 2

| Cover stock (pbw) | A   | B  | C  | D  | E   | F  |
|-------------------|-----|----|----|----|-----|----|
| Hytrel 4047       | 100 | -  | -  | -  | -   | -  |
| Surlyn 8120       | -   | 50 | -  | 30 | -   | -  |
| Himilan 1557      | -   | 50 | -  | -  | -   | 50 |
| Himilan 1856      | -   | -  | 90 | -  | -   | -  |
| NO825J            | -   | -  | 10 | -  | -   | -  |
| Himilan 1605      | -   | -  | -  | 20 | -   | 50 |
| Himilan 1706      | -   | -  | -  | 50 | -   | -  |
| PANDEX T-7890     | -   | -  | -  | -  | 100 | -  |

Hytrel 4047: Toray duPont K.K., polyester base thermoplastic elastomer

NO825J: Mitsui duPont K.K., ethylene/methacrylic acid/methacrylate  
5 terpolymer (nuclei)

Surlyn 8120: E. I. duPont, ionomer resin

Himilan 1557: Mitsui duPont Polymers K.K., ionomer resin

Himilan 1856: Mitsui duPont Polymers K.K., ionomer resin

Himilan 1605: Mitsui duPont Polymers K.K., ionomer resin

10 Himilan 1706: Mitsui duPont Polymers K.K., ionomer resin

PANDEX T-7890: Dai-Nihon Ink Chemical Industry K.K., thermoplastic  
polyurethane elastomer

Note that an appropriate amount of titanium dioxide  
15 was blended in resin compositions A to F.

Table 3

| Type | Diameter (mm) | Depth (mm) | V <sub>o</sub> | Number | V <sub>R</sub> (%) |
|------|---------------|------------|----------------|--------|--------------------|
| 1    | 4.100         | 0.195      | 0.440          | 32     | 0.89               |
|      | 4.200         | 0.195      | 0.440          | 40     |                    |
|      | 4.000         | 0.195      | 0.440          | 184    |                    |
|      | 3.900         | 0.195      | 0.440          | 16     |                    |
|      | 3.400         | 0.195      | 0.440          | 104    |                    |
|      | 3.350         | 0.195      | 0.440          | 16     |                    |
| 2    | 4.100         | 0.210      | 0.450          | 32     | 0.86               |
|      | 4.200         | 0.180      | 0.450          | 40     |                    |
|      | 4.000         | 0.165      | 0.450          | 184    |                    |
|      | 3.900         | 0.200      | 0.450          | 16     |                    |
|      | 3.400         | 0.155      | 0.450          | 104    |                    |
|      | 3.350         | 0.160      | 0.450          | 16     |                    |
| 3    | 3.850         | 0.160      | 0.500          | 288    | 0.80               |
|      | 3.250         | 0.150      | 0.500          | 72     |                    |
|      | 2.500         | 0.140      | 0.500          | 42     |                    |
| 4    | 3.850         | 0.175      | 0.525          | 288    | 0.93               |
|      | 3.250         | 0.170      | 0.530          | 72     |                    |
|      | 2.500         | 0.170      | 0.530          | 42     |                    |
| 5    | 4.000         | 0.160      | 0.480          | 114    | 0.77               |
|      | 4.000         | 0.180      | 0.480          | 42     |                    |
|      | 3.650         | 0.140      | 0.480          | 180    |                    |
|      | 3.600         | 0.140      | 0.480          | 24     |                    |
|      | 2.550         | 0.100      | 0.480          | 60     |                    |
| 6    | 3.900         | 0.150      | 0.470          | 240    | 0.66               |
|      | 3.200         | 0.150      | 0.470          | 120    |                    |
| 7    | 3.850         | 0.170      | 0.465          | 340    | 1.04               |
|      | 3.600         | 0.170      | 0.465          | 140    |                    |
| 8    | 3.850         | 0.185      | 0.460          | 340    | 1.12               |
|      | 3.600         | 0.185      | 0.460          | 140    |                    |

Table 4

| Solid core                                   | Composition   | E1   | E2   | E3   | E4   | E5                   |
|--|---|--|--|--|--|----------------------|
|  | Hardness* (mm)  | I  | II   | III  | IV   | V                    |
| Inner cover                                  | Stock   | A  | C  | D  | A  | B                    |
| layer  | Shore D hardness  | 40   | 49   | 55   | 40   | 58                   |
|  | Gage (mm)   | 1.5  | 1.5  | 1.5  | 1.5  | 1.5                  |
| Outer cover                                  | Stock   | B  | D  | B  | E  | F                    |
| layer  | Shore D hardness  | 58   | 55   | 58   | 42   | 60                   |
|  | Gage (mm)   | 1.5  | 1.5  | 1.5  | 1.5  | 1.5                  |
| Dimple type                                  |   | 1  | 2  | 3  | 4  | 5                    |
| Inner layer Shore D<br>x outer layer Shore D |   | 2320   | 2695   | 3190   | 1680   | 3480                 |
| V <sub>R</sub> (%)                           |   | 0.89   | 0.86   | 0.80   | 0.93   | 0.77                 |
| #W1/HS48                                     | Spin (rpm)  | 2530   | 2540   | 2450   | 2680   | 2250                 |
|  | Carry (m)   | 225  | 229  | 228  | 228  | 227                  |
|  | Total (m)   | 255  | 257  | 258  | 257  | 258                  |
| Trajectory                                   | somewhat rising,<br>long-lasting,<br>relatively low<br>trajectory | rising,<br>similar to<br>balata ball<br>trajectory | liner-like,<br>long-lasting,<br>medium<br>trajectory | rising,<br>similar to<br>balata ball<br>trajectory | liner-like,<br>long-lasting,<br>medium<br>trajectory | medium<br>trajectory |

\* a distortion (mm) of the solid core under an applied load of 100 kg

Table 5

| Solid core                                   | Composition                                      | CE1                                  | CE2                          | CE3  |
|--|--|--------------------------------------|------------------------------|------|
|  | Hardness* (mm)                                   | I                                    | III                          | IV   |
| Inner cover Stock                            | A  | D                                    | A                            |      |
| layer  | Shore D hardness                                 | 40                                   | 55                           | 40   |
|  | Gage (mm)  | 1.5                                  | 1.5                          | 1.5  |
| Outer cover Stock                            | B  | B                                    | E                            |      |
| layer  | Shore D hardness                                 | 58                                   | 58                           | 42   |
|  | Gage (mm)  | 1.5                                  | 1.5                          | 1.5  |
| Dimple type                                  | 6  | 7                                    | 8                            |      |
| Inner layer Shore D<br>x outer layer Shore D | 2320   | 3190                                 | 1680                         |      |
| V <sub>R</sub> (%)                           | 0.73   | 1.04                                 | 1.12                         |      |
| #W1/HS48                                     | Spin (rpm)                                       | 2530                                 | 2450                         | 2680 |
|  | Carry (m)  | 220                                  | 218                          | 217  |
|  | Total (m)  | 247                                  | 243                          | 245  |
| Trajectory                                   | liner-like, high<br>liner-like,<br>low, dropping | liner-like,<br>high<br>low, dropping | liner-like,<br>low, dropping |      |

\* a distortion (mm) of the solid core under an applied load of 100 kg

As seen from the results of Examples, the multi-piece solid golf balls of the invention exhibit a satisfactory trajectory and are excellent in all of spin, carry, and total flight distance.

5        In contrast, the multi-piece solid golf ball of Comparative Example 1 wherein  $V_R$  is below the specified range associated with the product of the Shore D hardnesses of the inner and outer cover layers was inferior in flight distance performance. The multi-piece  
10      solid golf balls of Comparative Examples 2 and 3 wherein  $V_R$  is above the specified range was inferior in flight distance performance and exhibited a dropping trajectory.